

Mixed-Integer Nonlinear Optimization for District Heating Network Expansion

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Trier University

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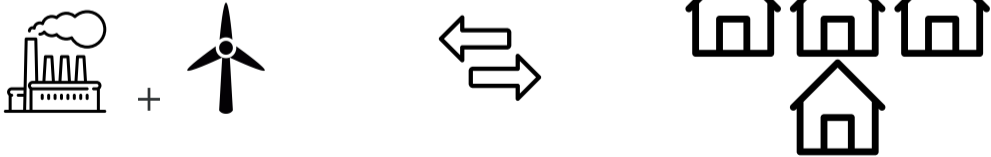
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⇒ District Heating Networks

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Optimization:

- Control (Benonysson et al. 1995; Krug et al. 2020; Sandou et al. 2005; Verrilli et al. 2017)
- Design (Ameri and Besharati 2016; Blommaert et al. 2018; Bracco et al. 2013; Guelpa et al. 2018; Mertz et al. 2017; Söderman 2007)
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Challenges:

- Nonlinear behaviour of fluids in pipes
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Assumptions:

- One dimensional stationary model
- Only tree shaped networks

Prologue

Modeling

Problem Formulation

Network and Physics Modeling

Thermal Energy Equation Approximation

Candidate Pipe Modeling

Numerical Results

Test Case

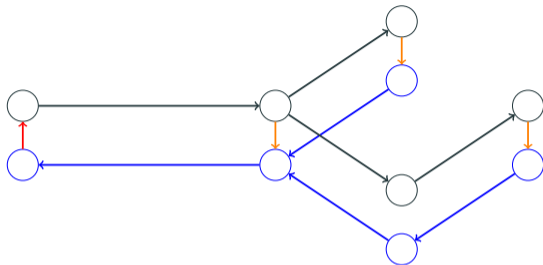
Initial Results

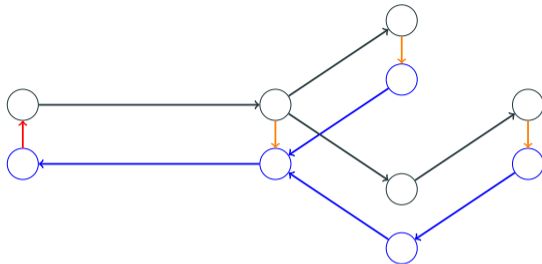
Discussion

Conclusion

max Profit = Consumer Payment - Expansion, Operation and Maintenance Cost
s.t. System physics,
Consumer constraints,
Depot constraints.

Network Modeling and Notation

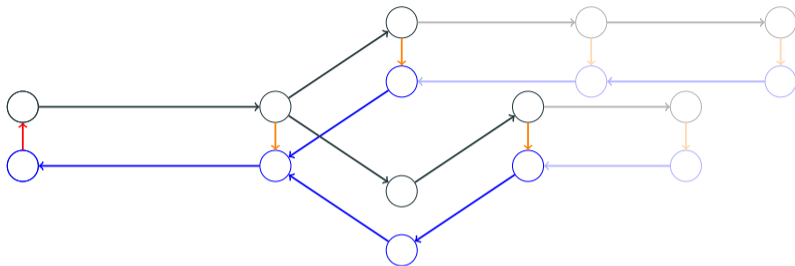




We introduce the graph $G = (V, A)$ such that:

- A_{ff}, A_{bf}, A_c, a_d
- V_{ff}, V_{bf}

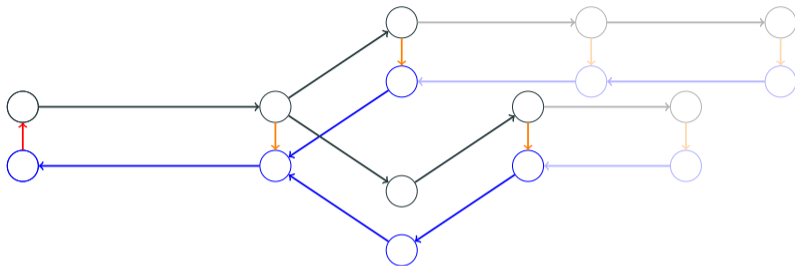
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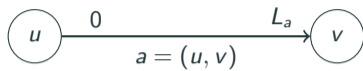
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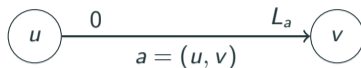
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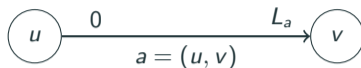
- A_{ff}, A_{bf}, A_c, a_d
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- $A_{ff}^e, A_{ff}^c, A_{bf}^e, A_{bf}^c, A_c^e, A_c^c$
- $V_{ff}^e, V_{ff}^c, V_{bf}^e, V_{bf}^c$





One-dimensional stationary momentum equation for compressible fluids in cylindrical pipes (Hauschild et al. 2020; Krug et al. 2020):

$$\frac{p_a(L_a) - p_a(0)}{L_a} = -g\rho h'_a - \lambda_a \frac{|v_a|v_a\rho}{2D_a}, \quad \forall a \in A_{\text{ff}} \cup A_{\text{bf}},$$

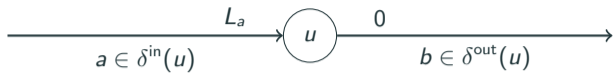


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One-dimensional stationary thermal energy equation:

$$T_a(L_a; v_a) = \begin{cases} T_{\text{soil}}, & v_a = 0 \\ (T_a(0) - T_{\text{soil}}) e^{-\frac{4U_a L_a}{c_p \rho D_a v_a}} + T_{\text{soil}}, & v_a > 0 \end{cases}, \quad \forall a \in A_{\text{ff}} \cup A_{\text{bf}}.$$





Mass flow continuity:

$$\sum_{a \in \delta^{\text{in}}(u)} q_a = \sum_{a \in \delta^{\text{out}}(u)} q_a, \quad u \in V.$$



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$$p_u = p_a(L_a), \quad u \in V, \quad a \in \delta^{\text{in}}(u).$$



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Temperature mixing (Krug et al. 2020):

$$T_u = \frac{\sum_{a \in \delta^{\text{in}}(u)} c_p q_a T_a(L_a)}{\sum_{a \in \delta^{\text{in}}(u)} c_p q_a}, \quad u \in V,$$

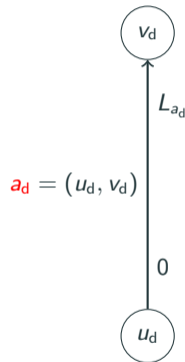
$$T_u = T_a(0), \quad u \in V, \quad a \in \delta^{\text{out}}(u).$$

For $\mathbf{a}_d = (u_d, v_d)$:

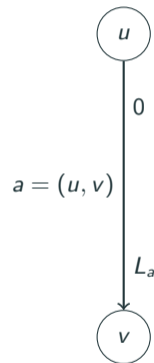
$$p_{u_d} = p_s,$$

$$P_p = \frac{q_{a_d}}{\rho} (p_{v_d} - p_{u_d}),$$

$$P_w + P_g = q_{a_d} c_p (T_a(L_{a_d}) - T_a(0)).$$



$$\begin{aligned}
 P_a &= q_a c_p (T_a(0) - T_a(L_a)), & a \in A_c^e, \\
 x_a P_a &= q_a c_p (T_a(0) - T_a(L_a)), & a \in A_c^c, \\
 T_a(L_a) &= T^{bf}, & a \in A_c^e \cup A_c^c, \\
 T_a(0) &\geq T_a^{ff}, & a \in A_c^e \cup A_c^c, \\
 p_v &\leq p_u, & a \in A_c^e \cup A_c^c.
 \end{aligned}$$



$$f(v_a, T_a(0), T_a(L_a)) := \begin{cases} (T_a(0) - T_{\text{soil}}) e^{-\frac{4U_a L_a}{c_p \rho D_a v_a}} + T_{\text{soil}} - T_a(L_a), & v_a > 0, \\ T_{\text{soil}} - T_a(L_a), & v_a = 0. \end{cases}$$

Thermal Energy Equation Approximation I

$$f(v_a, T_a(0), T_a(L_a)) := \begin{cases} (T_a(0) - T_{\text{soil}}) e^{-\frac{4U_a L_a}{c_p \rho D_a v_a}} + T_{\text{soil}} - T_a(L_a), & v_a > 0, \\ T_{\text{soil}} - T_a(L_a), & v_a = 0. \end{cases}$$

⇓

$$f_{\text{approx}}(v_a, T_a(0), T_a(L_a)) := \sum_{(k,l,m) \in \Theta_d} \alpha_{klm} v_a^k T_a(0)^l T_a(L_a)^m + T_a(L_a) - T_{\text{soil}},$$

with

$$\Theta_d := \left\{ (k, l, m) \in \mathbb{N}^3 : k \neq 0 \text{ and } k + l + m \leq d \right\}.$$

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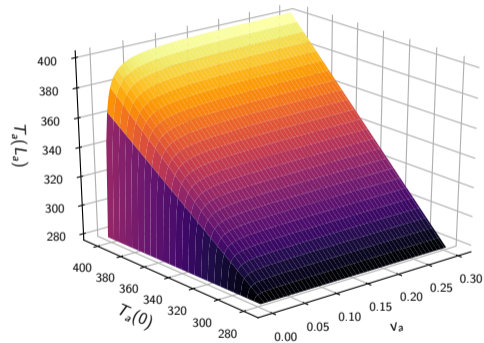
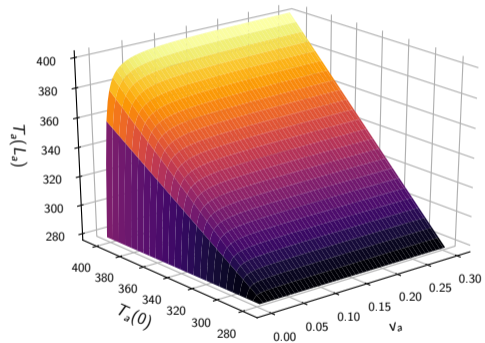
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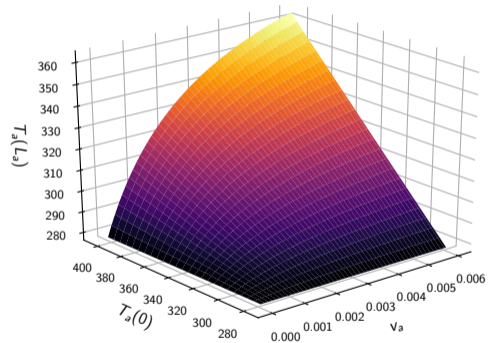
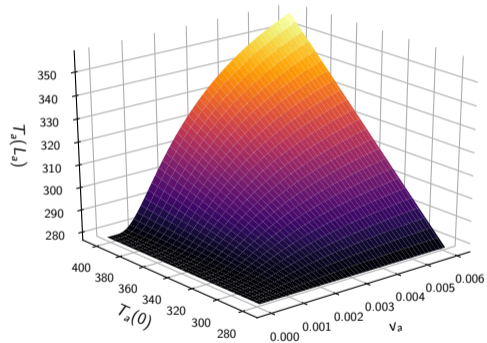


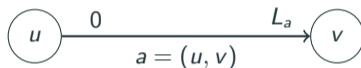
$$\min_{\alpha} \sum_{i \in I} f_{\text{approx}}(v_a^i, T_a(0)^i, T_a(L_a)^i)^2.$$

Thermal Energy Equation Approximation II



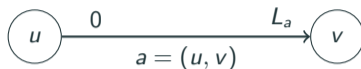
Thermal Energy Equation Approximation III





One-dimensional stationary momentum equation for compressible fluids in cylindrical pipes:

$$p_v - p_u + L_a g \rho h'_a + \lambda_a \frac{|v_a| v_a \rho L_a}{2D_a} = 0, \quad \forall a \in A_{\text{ff}} \cup A_{\text{bf}}.$$



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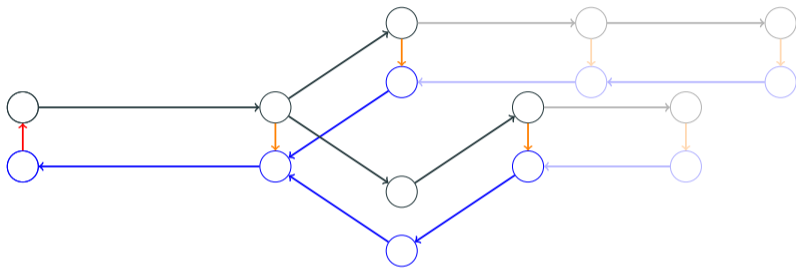
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And,

$$p_v - p_u + L_a g \rho h'_a + \lambda_a \frac{|v_a| v_a \rho L_a}{2D_a} \leq (1 - x_a) M_a^1, \quad \forall a = (u, v) \in A_{\text{ff}}^c \cup A_{\text{bf}}^c,$$

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Candidate Pipe Modeling: Valid Inequalities

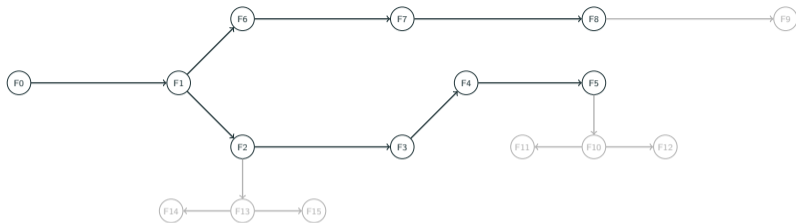


Objective

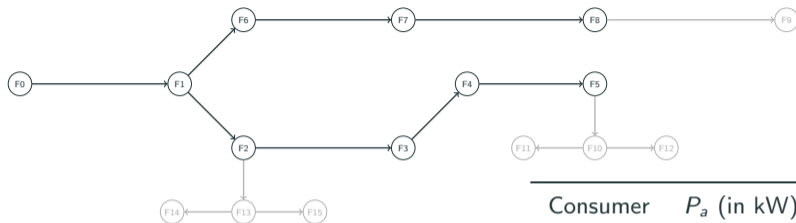
$$\max \sum_{a \in A_{\xi}^c} P_a w \pi x_a - \sum_{a \in A_{ff}^c \cup A_{bf}^c \cup A_{\xi}^c} C_a^{\text{inv}} x_a - w (C_p P_p + C_w P_w + C_g P_g)$$

max objective,
s.t. stationary incompressible Euler equation,
stationary thermal energy equation approximation,
mass conservation,
pressure continuity,
temperature mixing equations,
depot constraints,
consumer constraints,
system bounds,
power bounds,
valid binary inequalities.

Test Case



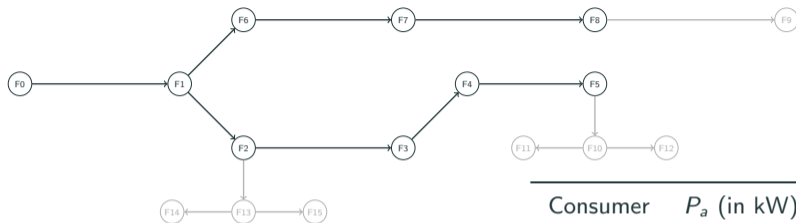
Test Case



Cost	C_w	C_g	C_p
Value (€/kWh)	0	0.0415	0.165
Edge	$a \in A_c^c$	$a \in A_{ff}^c \cup A_{bf}^c$	
C_a^{inv} (€)	100 000	[90 000, 330 000]	

Consumer	P_a (in kW)
(F2,B2)	200.00
(F3,B3)	600.00
(F5,B5)	150.00
(F6,B6)	666.66
(F8,B8)	200.00
(F9,B9)	183.33
(F11,B11)	183.33
(F12,B12)	183.33
(F14,B14)	183.33
(F15,B15)	183.33

Test Case

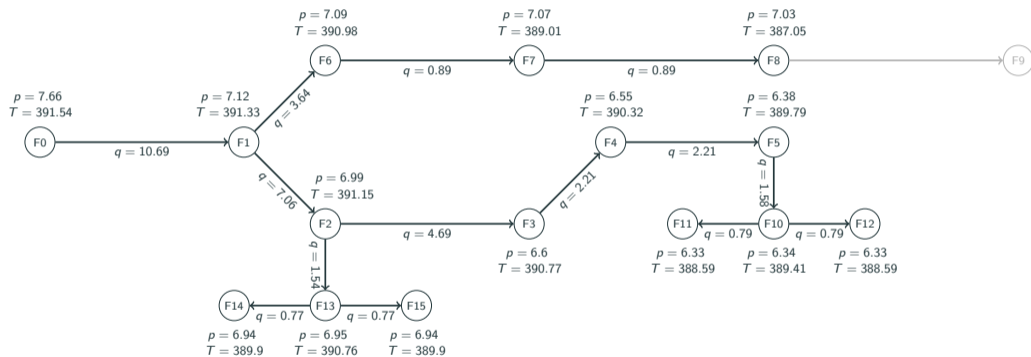


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Intel(R) Core(TM) i7-8550U, 16 GB RAM.
ANTIGONE using the Pyomo interface.

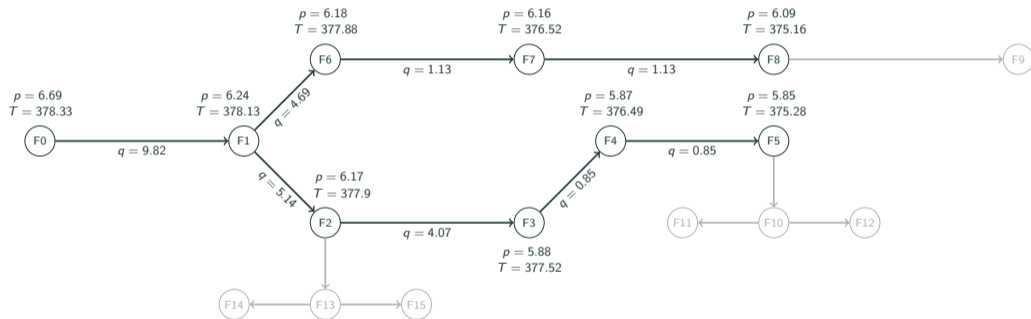
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Initial Results



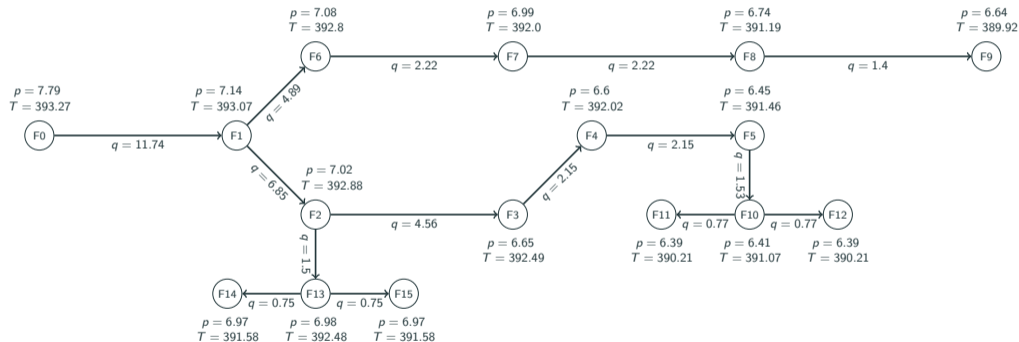
Discussion: Impact of Estimated Average Demand

If $P_a = 150$ kW for all $a \in A_c$:



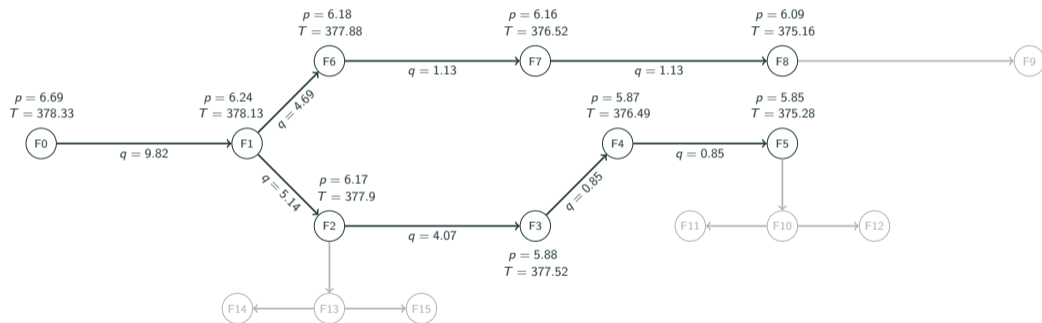
Discussion: Impact of Distance

If $P_a = 350$ kW for all $a \in A_c^c$:



Discussion: Impact of Thermal Losses

If $U_a = 0.5 \text{ W m}^{-1} \text{ K}^{-2} \Rightarrow 0.8 \text{ W m}^{-1} \text{ K}^{-2}$:



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- Nonlinear modeling of T and p behavior

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- Polynomial approximation of the Thermal Energy Equation

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Main parameters:

- Estimated average demand
- Distance of the candidate consumer
- Pipe insulation